

1.1nV/ $\sqrt{\text{Hz}}$ 噪声、低功耗、精准 运算放大器

查询样品: [OPA211-EP](#)

特性

- 低电压噪声: **1kHz** 时为 **1.1nV/ $\sqrt{\text{Hz}}$**
- 输入电压噪声:
80nV_{PP} (0.1Hz 至 10Hz)
- 总谐波失真 (THD)+N: **-136dB** (G=1, f=1kHz)
- 偏移电压: **180 μV** (最大值)
- 偏移电压漂移: **0.35 $\mu\text{V}/^\circ\text{C}$** (典型值)
- 低电源电流: 每通道 **3.6mA** (典型值)
- 单位增益稳定
- 增益带宽产品:
80MHz (G=100)
45MHz (G=1)
- 转换率: **27V/ μs**
- **16 位** 稳定时间: **700ns**
- 宽电源范围:
 $\pm 2.25\text{V}$ 至 $\pm 18\text{V}$, 或者 **+4.5V 至 +36V**
- 轨至轨输出
- 输出电流: **30 mA**

应用范围

- 锁相环路 (PLL) 环路滤波器
- 低噪声、低功耗信号处理
- **16 位** 模数转换器 (ADC) 驱动器
- 数模转换器 (DAC) 输出放大器
- 有源滤波器
- 低噪声仪器放大器
- 超声波放大器
- 专业音频前置放大器
- 低噪声频率合成器
- 红外检测器放大器
- 水听器放大器
- 地音听器放大器
- 医疗应用

支持国防、航空航天、和医疗应用

- 受控基线
 - 一个组装/测试场所
 - 一个制造场所
 - 军用温度范围 (**-55 $^\circ\text{C}$ /125 $^\circ\text{C}$**) 内可用 ⁽¹⁾
 - 延长的产品使用寿命周期
 - 延长产品的变更通知
 - 产品追溯性
- (1) 可提供额外温度范围-请与厂家联系

说明

OPA211 系列精准运算放大器用一个只有 3.6mA 的电源电流实现极低 1.1nV/ $\sqrt{\text{Hz}}$ 噪声密度。这个系列产品还提供轨到轨输出摆幅, 这大大增加了动态范围。

OPA211 系列产品极低的电压和低电流噪声、高速度、和宽输出摆幅使得这些器件成为 PLL 应用中环路滤波放大器的出色选择。

在精准数据采集应用中, OPA211 运算放大器系列产品在整个 10V 输出摆幅内实现 16 位精度所需的稳定时间为 700ns。这个交流性能, 与温度范围内只有 125 μV 的偏移和 0.35 $\mu\text{V}/^\circ\text{C}$ 的漂移组合在一起, 使得 OPA211 成为驱动高精度 16 位模数转换器 (ADC) 或者缓冲高分辨率数模转换器 (DAC) 输出的理想选择。

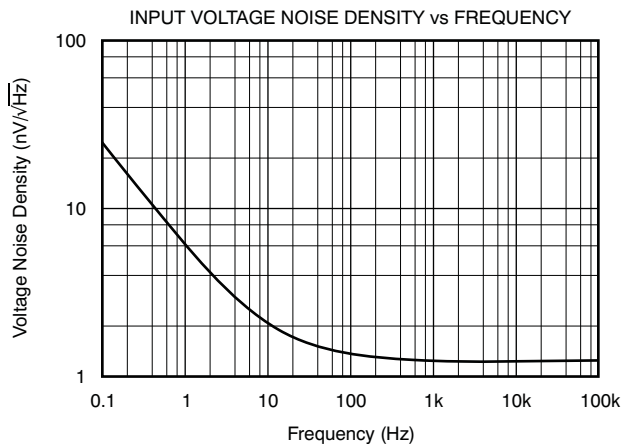
OPA211 可在 $\pm 2.25\text{V}$ 至 $\pm 18\text{V}$ 的宽双电源范围, 或者 +4.5V 至 +36V 的单电源范围内运行。

OPA211 采用小型微型小外形尺寸 (MSOP)-8 封装。这个运算放大器的额定温度范围 $T_A = -55^\circ\text{C}$ 至 +125 $^\circ\text{C}$ 。



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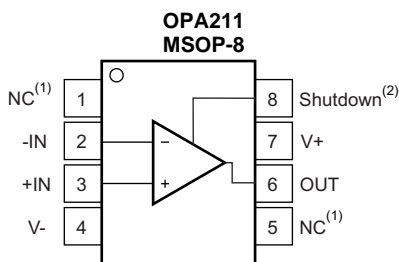


PACKAGE/ORDERING INFORMATION⁽¹⁾

T _A	PACKAGE	ORDERABLE PART NUMBER	PACKAGE MARKING	VID NUMBER
-55°C to 125°C	MSOP-8 - DGK	OPA211MDGKTEP	OBCM	V62/12619-01XE

(1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or visit the device product folder at www.ti.com.

PIN CONFIGURATIONS



(1) NC denotes no internal connection.

(2) Shutdown function:

- Device enabled: $(V-) \leq V_{\text{SHUTDOWN}} \leq (V+) - 3V$
- Device disabled: $V_{\text{SHUTDOWN}} \geq (V+) - 0.35V$



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

ABSOLUTE MAXIMUM RATINGS⁽¹⁾

Over operating free-air temperature range (unless otherwise noted).

		VALUE	UNIT
Supply Voltage	$V_S = (V+) - (V-)$	40	V
Input Voltage		$(V-) - 0.5$ to $(V+) + 0.5$	V
Input Current (Any pin except power-supply pins)		± 10	mA
Output Short-Circuit ⁽²⁾		Continuous	
Operating Temperature	(T_A)	-55 to +125	°C
Storage Temperature	(T_A)	-65 to +150	°C
Junction Temperature	(T_J)	200	°C
ESD Ratings	Human Body Model (HBM)	3000	V
	Charged Device Model (CDM)	1000	V

- (1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not supported.
- (2) Short-circuit to $V_S/2$ (ground in symmetrical dual supply setups), one amplifier per package.

THERMAL INFORMATION

THERMAL METRIC ⁽¹⁾		OPA211	UNITS
		DGK	
		8 PINS	
θ_{JA}	Junction-to-ambient thermal resistance ⁽²⁾	184.9	°C/W
θ_{JCTop}	Junction-to-case (top) thermal resistance ⁽³⁾	71.2	
θ_{JB}	Junction-to-board thermal resistance ⁽⁴⁾	104.9	
Ψ_{JT}	Junction-to-top characterization parameter ⁽⁵⁾	11.5	
Ψ_{JB}	Junction-to-board characterization parameter ⁽⁶⁾	103.4	
θ_{JCbott}	Junction-to-case (bottom) thermal resistance ⁽⁷⁾	N/A	

- (1) 有关传统和全新热量的更多信息，请参阅 *IC 封装热量量* 应用报告 (文献号: SPRA953)。
- (2) 在 JESD51-2a 描述的环境中，按照 JESD51-7 的规定，在一个 JEDEC 标准高 K 电路板上进行仿真，从而获得自然对流条件下的结至环境热阻抗。
- (3) 通过在封装顶部模拟一个冷板测试来获得结至芯片外壳 (顶部) 的热阻。不存在特定的 JEDEC 标准测试，但可在 ANSI SEMI 标准 G30-88 中找到内容接近的说明。
- (4) 按照 JESD51-8 中的说明，通过在配有用于控制 PCB 温度的环形冷板夹具的环境中进行仿真，以获得结至电路板的热阻。
- (5) 结至顶部的特征参数，(Ψ_{JT})，估算真实系统中器件的结温，并使用 JESD51-2a (第 6 章和第 7 章) 中描述的程序从仿真数据中提取出该参数以便获得 θ_{JA} 。
- (6) 结至电路板的特征参数，(Ψ_{JB})，估算真实系统中器件的结温，并使用 JESD51-2a (第 6 章和第 7 章) 中描述的程序从仿真数据中提取出该参数以便获得 θ_{JA} 。
- (7) 通过在外露 (电源) 焊盘上进行冷板测试仿真来获得结至芯片外壳 (底部) 热阻。不存在特定的 JEDEC 标准测试，但可在 ANSI SEMI 标准 G30-88 中找到了内容接近的说明。

ELECTRICAL CHARACTERISTICS: $V_S = \pm 2.25V$ to $\pm 18V$

BOLDFACE limits apply over the specified temperature range, $T_A = -55^\circ\text{C}$ to $+125^\circ\text{C}$.

At $T_A = +25^\circ\text{C}$, $R_L = 10\text{k}\Omega$ connected to midsupply, $V_{CM} = V_{OUT} = \text{midsupply}$, unless otherwise noted.

PARAMETER	CONDITIONS	MIN	TYP	MAX	UNIT
OFFSET VOLTAGE					
Input Offset Voltage	V_{OS} $V_S = \pm 15V$		± 20	± 100	μV
Over Temperature				± 180	μV
Drift	dV_{OS}/dT		0.35		$\mu\text{V}/^\circ\text{C}$
vs Power Supply	PSRR $V_S = \pm 2.25V$ to $\pm 18V$		0.1	0.5	$\mu\text{V}/\text{V}$
Over Temperature				3	$\mu\text{V}/\text{V}$
INPUT BIAS CURRENT					
Input Bias Current	I_B $V_{CM} = 0V$		± 50	± 200	nA
Offset Current	I_{OS} $V_{CM} = 0V$		± 20	± 150	nA
NOISE					
Input Voltage Noise	e_n $f = 0.1\text{Hz}$ to 10Hz		80		nV_{PP}
Input Voltage Noise Density	$f = 10\text{Hz}$		2		$\text{nV}/\sqrt{\text{Hz}}$
	$f = 100\text{Hz}$		1.4		$\text{nV}/\sqrt{\text{Hz}}$
	$f = 1\text{kHz}$		1.1		$\text{nV}/\sqrt{\text{Hz}}$
Input Current Noise Density	I_n $f = 10\text{Hz}$		3.2		$\text{pA}/\sqrt{\text{Hz}}$
	$f = 1\text{kHz}$		1.7		$\text{pA}/\sqrt{\text{Hz}}$
INPUT VOLTAGE RANGE					
Common-Mode Voltage Range	V_{CM} $V_S \geq \pm 5V$ $V_S < \pm 5V$	$(V-) + 1.8$ $(V-) + 2$		$(V+) - 1.4$ $(V+) - 1.4$	V V
Common-Mode Rejection Ratio	CMRR $V_S \geq \pm 5V, (V-) + 2V \leq V_{CM} \leq (V+) - 2V$ $V_S < \pm 5V, (V-) + 2V \leq V_{CM} \leq (V+) - 2V$	114 108	120 120		dB dB
INPUT IMPEDANCE					
Differential			$20\text{k} \parallel 8$		$\Omega \parallel \text{pF}$
Common-Mode			$10^9 \parallel 2$		$\Omega \parallel \text{pF}$
OPEN-LOOP GAIN					
Open-Loop Voltage Gain	A_{OL} $(V-) + 0.2V \leq V_O \leq (V+) - 0.2V,$ $R_L = 10\text{k}\Omega$	114	130		dB
	A_{OL} $(V-) + 0.6V \leq V_O \leq (V+) - 0.6V,$ $R_L = 600\Omega$	110	114		dB
Over Temperature	A_{OL} $(V-) + 0.6V \leq V_O \leq (V+) - 0.6V,$ $I_O \leq 15\text{mA}$	110			dB
	A_{OL} $(V-) + 0.6V \leq V_O \leq (V+) - 0.6V,$ $15\text{mA} < I_O \leq 30\text{mA}$	103			dB
FREQUENCY RESPONSE					
Gain-Bandwidth Product	GBW $G = 100$ $G = 1$		80 45		MHz MHz
Slew Rate	SR		27		$\text{V}/\mu\text{s}$
Settling Time, 0.01%	t_S $V_S = \pm 15V, G = -1, 10V$ Step, $C_L = 100\text{pF}$		400		ns
0.0015% (16-bit)	$V_S = \pm 15V, G = -1, 10V$ Step, $C_L = 100\text{pF}$		700		ns
Overload Recovery Time	$G = -10$		500		ns
Total Harmonic Distortion + Noise	THD+N $G = +1, f = 1\text{kHz},$ $V_O = 3V_{RMS}, R_L = 600\Omega$		0.000015		%
			-136		dB

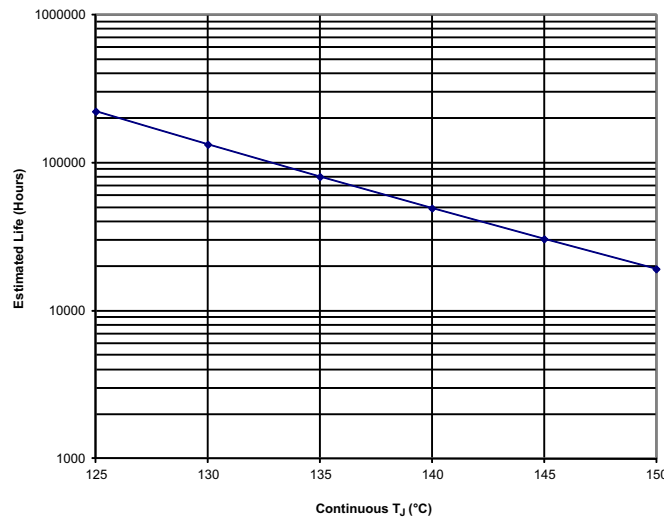
ELECTRICAL CHARACTERISTICS: $V_S = \pm 2.25V$ to $\pm 18V$ (continued)

BOLDFACE limits apply over the specified temperature range, $T_A = -55^\circ C$ to $+125^\circ C$.

At $T_A = +25^\circ C$, $R_L = 10k\Omega$ connected to midsupply, $V_{CM} = V_{OUT} =$ midsupply, unless otherwise noted.

PARAMETER	CONDITIONS	MIN	TYP	MAX	UNIT
OUTPUT					
Voltage Output	V_{OUT} $R_L = 10k\Omega, A_{OL} \geq 114dB$ $R_L = 600\Omega, A_{OL} \geq 110dB$ $I_o < 15mA, A_{OL} \geq 110dB$	(V-) + 0.2		(V+) - 0.2	V
		(V-) + 0.6		(V+) - 0.6	V
		(V-) + 0.6		(V+) - 0.6	V
Short-Circuit Current	I_{SC}		+30/-45		mA
Capacitive Load Drive	C_{LOAD}	See Typical Characteristics			pF
Open-Loop Output Impedance	Z_O	f = 1MHz			Ω
SHUTDOWN					
Shutdown Pin Input Voltage ⁽¹⁾	Device disabled (shutdown) Device enabled	(V+) - 0.35		(V+) - 3	V
					V
Shutdown Pin Leakage Current			1		μA
Turn-On Time ⁽²⁾			2		μs
Turn-Off Time ⁽²⁾			3		μs
Shutdown Current	Shutdown (disabled)		1	20	μA
POWER SUPPLY					
Specified Voltage	V_S	± 2.25		± 18	V
Quiescent Current (per channel)	I_Q	$I_{OUT} = 0A$	3.6	4.5	mA
					6
TEMPERATURE RANGE					
Operating Range	T_A	-55		+125	$^\circ C$
Thermal Resistance	θ_{JA}		200		$^\circ C/W$

- (1) When disabled, the output assumes a high-impedance state.
- (2) See [Typical Characteristic](#) curves, [Figure 42](#) through [Figure 44](#).



- A. See datasheet for absolute maximum and minimum recommended operating conditions.
- B. Silicon operating life design goal is 10 years at $105^\circ C$ junction temperature (does not include package interconnect life).

Figure 1. OPA211-EP Wirebond Life Derating Chart

TYPICAL CHARACTERISTICS

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.

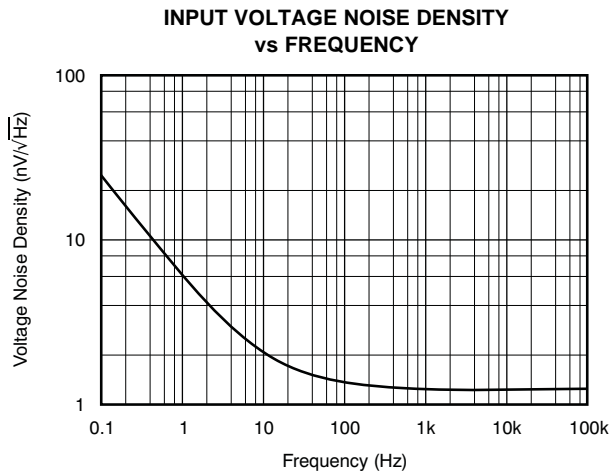


Figure 2.

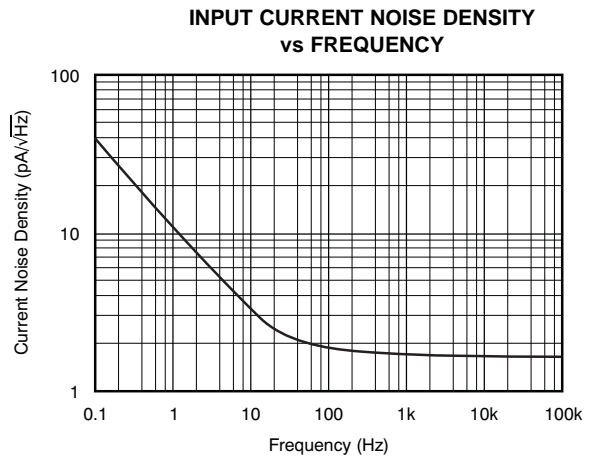


Figure 3.

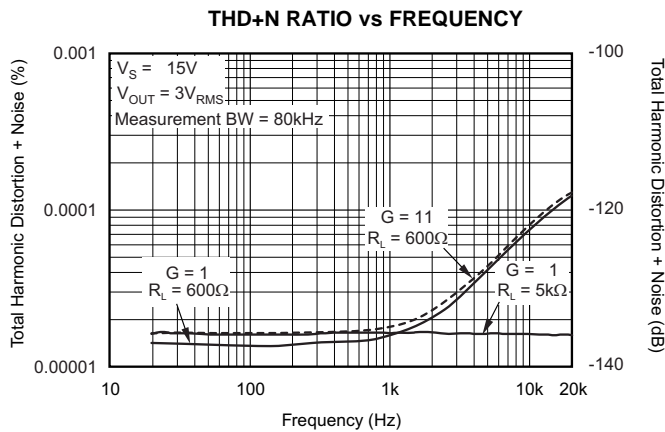


Figure 4.

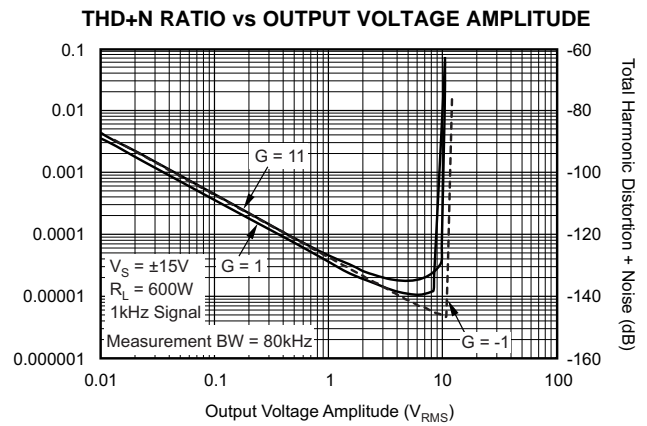


Figure 5.

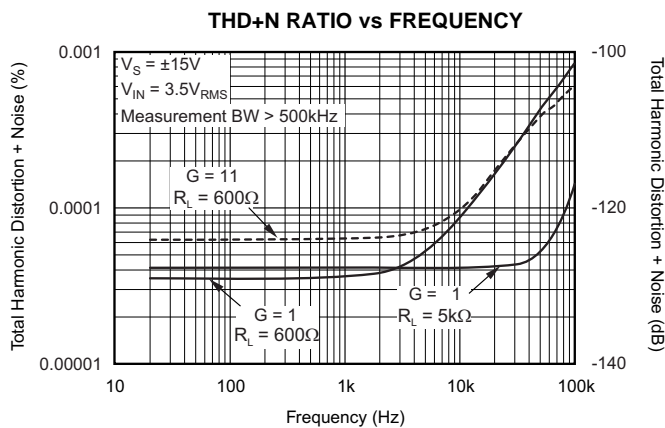


Figure 6.

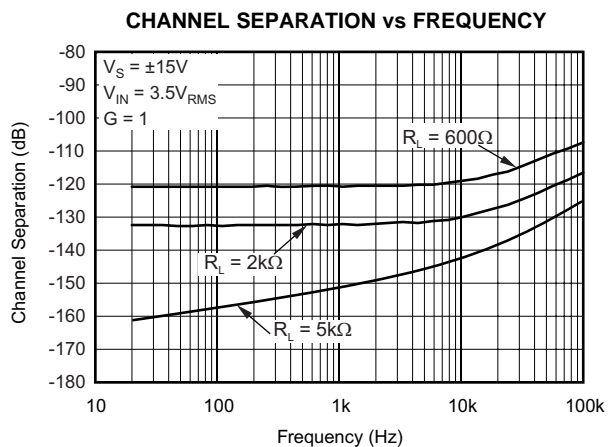


Figure 7.

TYPICAL CHARACTERISTICS (continued)

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.

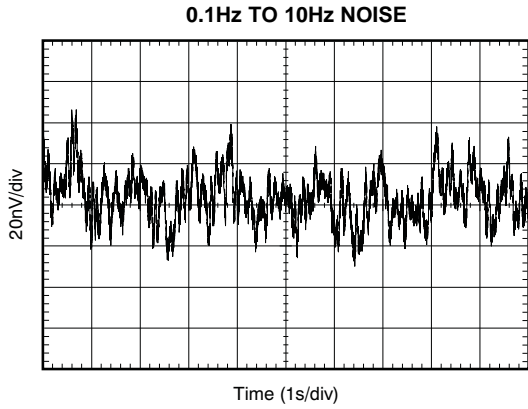


Figure 8.

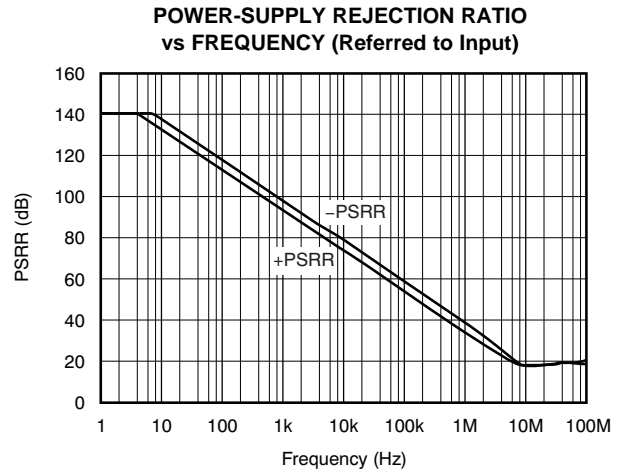


Figure 9.

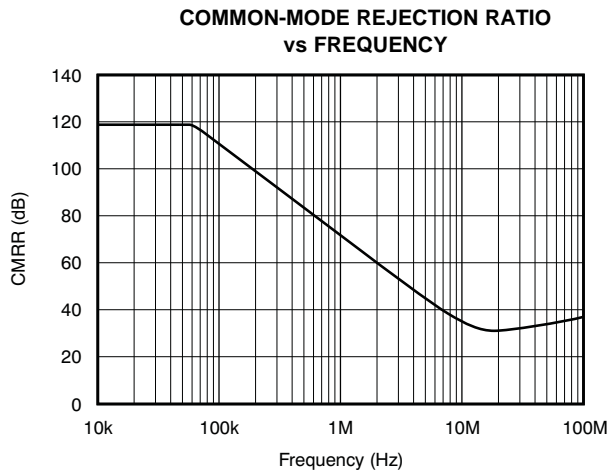


Figure 10.

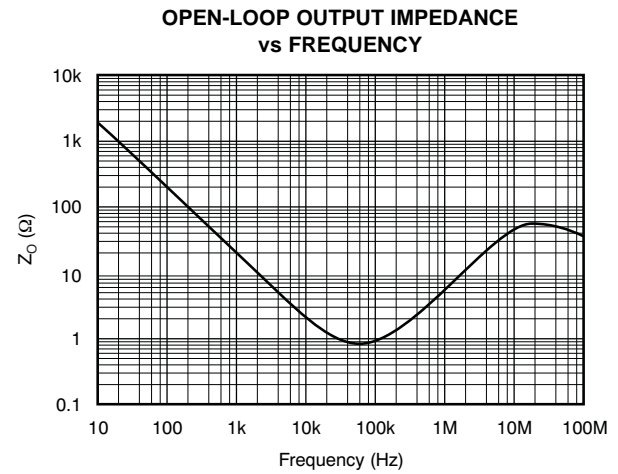


Figure 11.

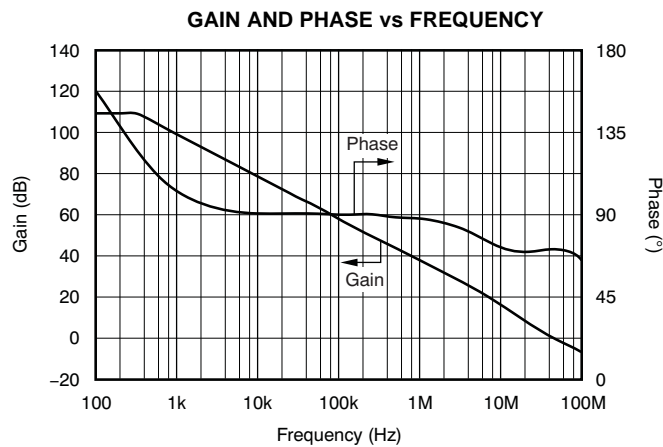


Figure 12.

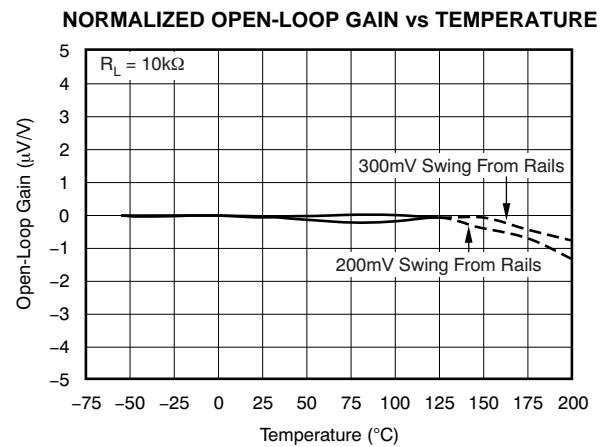


Figure 13.

TYPICAL CHARACTERISTICS (continued)

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.

OFFSET VOLTAGE PRODUCTION DISTRIBUTION

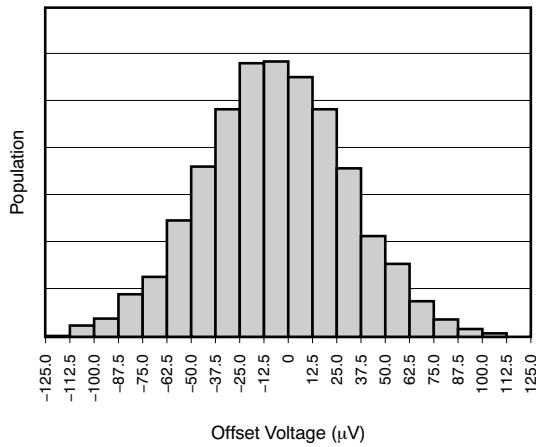


Figure 14.

OFFSET VOLTAGE DRIFT PRODUCTION DISTRIBUTION

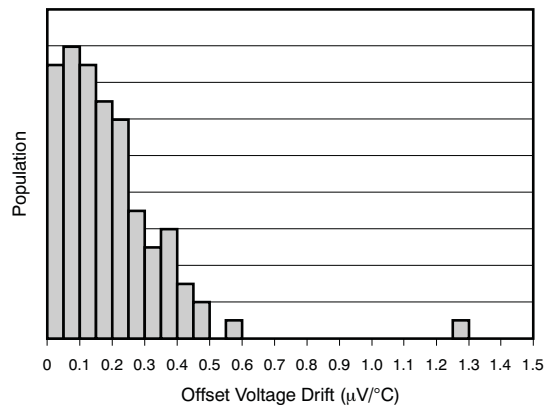


Figure 15.

I_B AND I_{OS} CURRENT vs TEMPERATURE

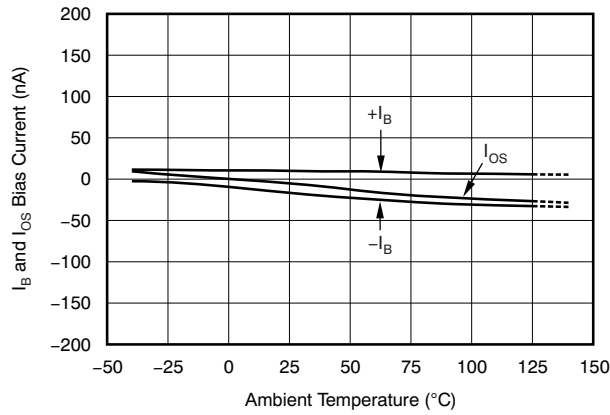


Figure 16.

OFFSET VOLTAGE vs COMMON-MODE VOLTAGE

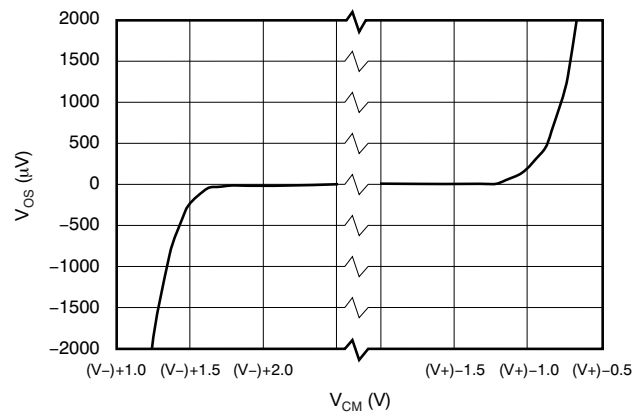


Figure 17.

V_{OS} WARMUP

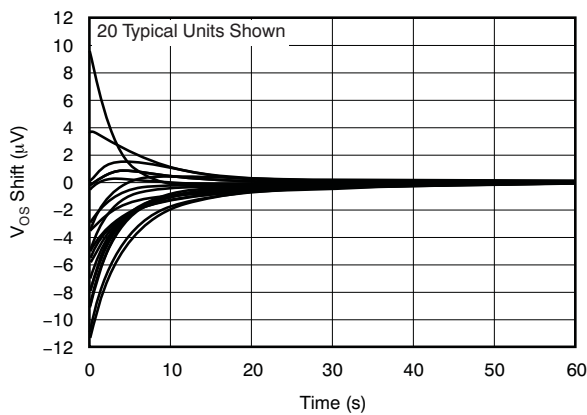


Figure 18.

INPUT OFFSET CURRENT vs SUPPLY VOLTAGE

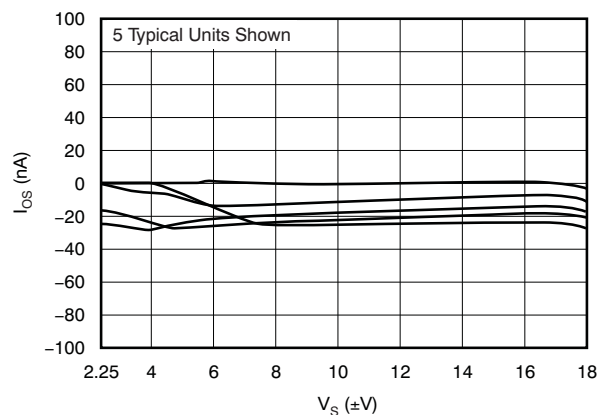


Figure 19.

TYPICAL CHARACTERISTICS (continued)

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.

INPUT OFFSET CURRENT vs COMMON-MODE VOLTAGE

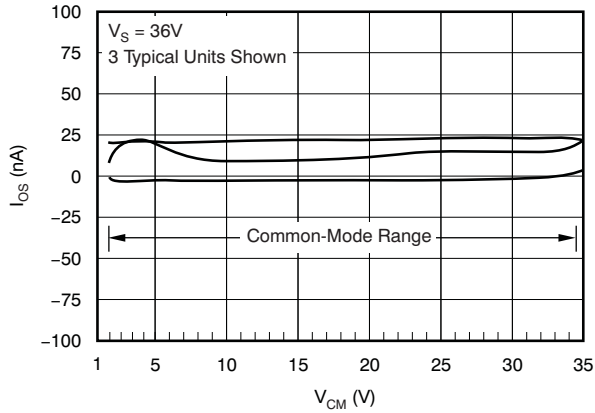


Figure 20.

INPUT BIAS CURRENT vs SUPPLY VOLTAGE

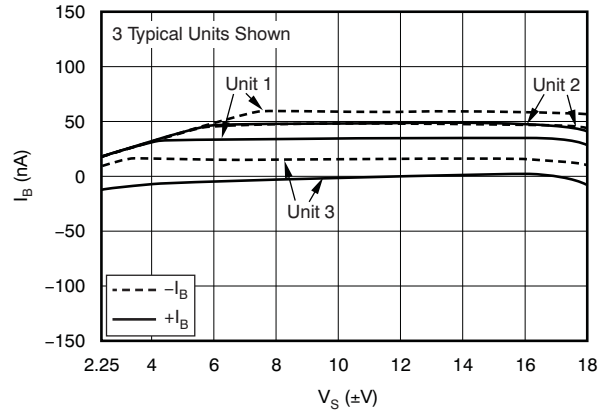


Figure 21.

INPUT BIAS CURRENT vs COMMON-MODE VOLTAGE

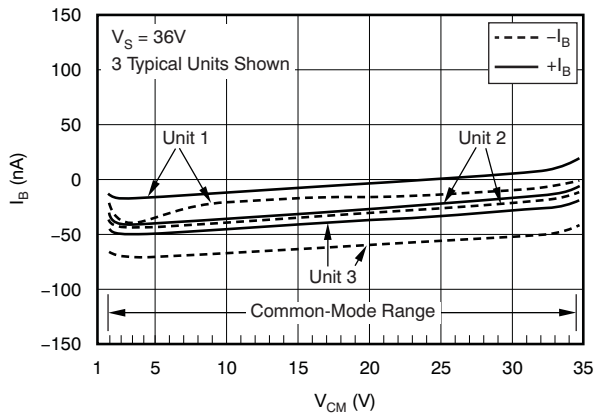


Figure 22.

QUIESCENT CURRENT vs TEMPERATURE

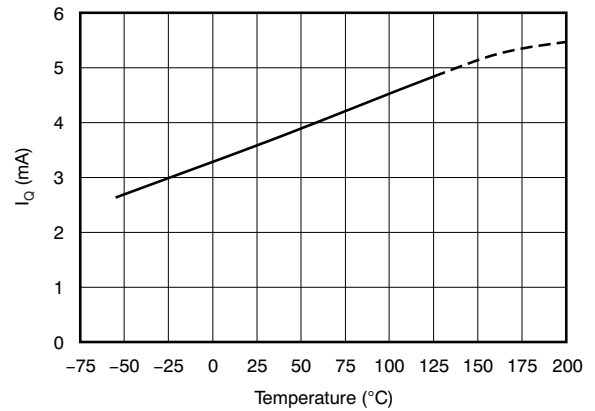


Figure 23.

QUIESCENT CURRENT vs SUPPLY VOLTAGE

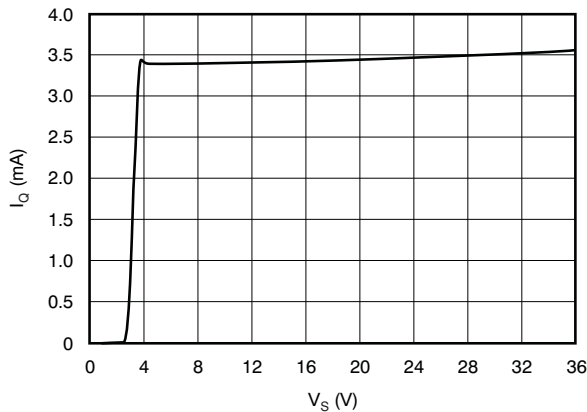


Figure 24.

NORMALIZED QUIESCENT CURRENT vs TIME

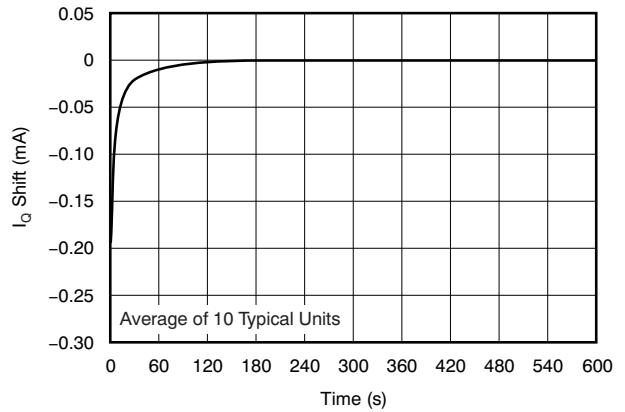


Figure 25.

TYPICAL CHARACTERISTICS (continued)

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.

SHORT-CIRCUIT CURRENT vs TEMPERATURE

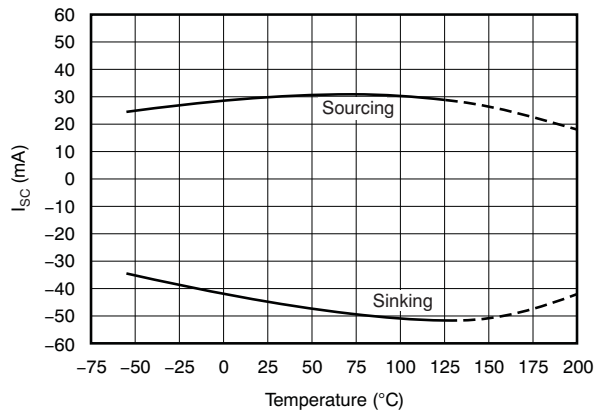


Figure 26.

SMALL-SIGNAL STEP RESPONSE (100mV)

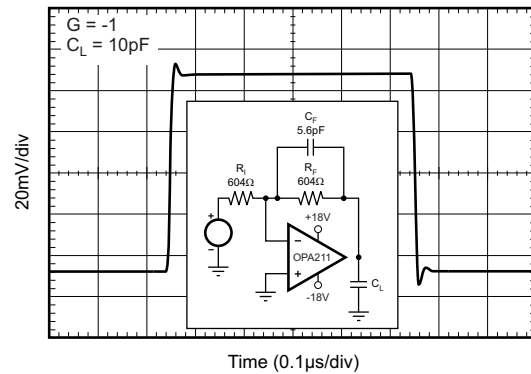


Figure 27.

SMALL-SIGNAL STEP RESPONSE (100mV)

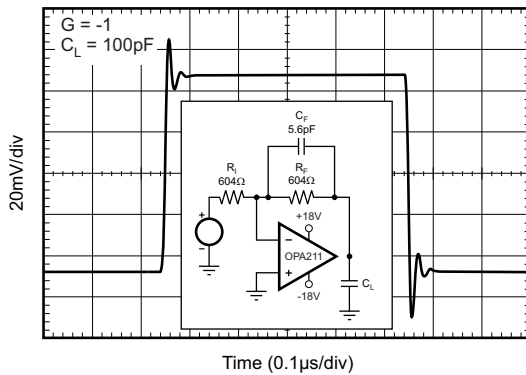


Figure 28.

SMALL-SIGNAL STEP RESPONSE (100mV)

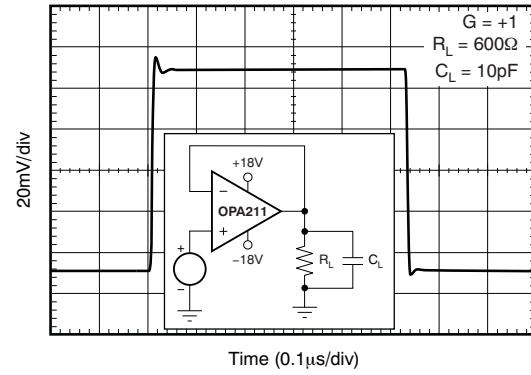


Figure 29.

SMALL-SIGNAL STEP RESPONSE (100mV)

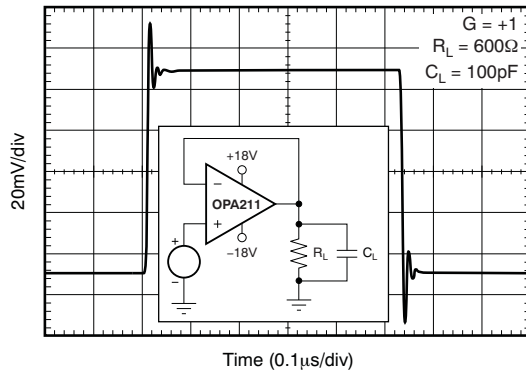


Figure 30.

SMALL-SIGNAL OVERSHOOT vs CAPACITIVE LOAD (100mV Output Step)

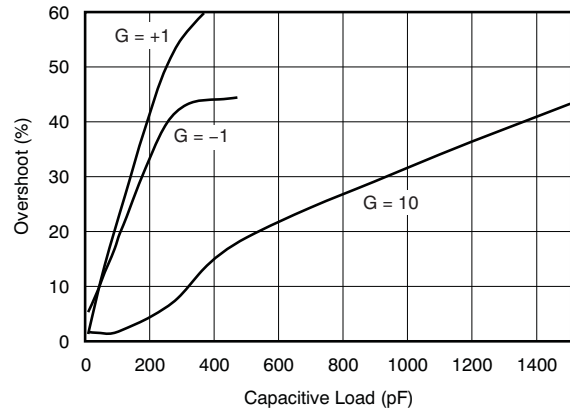


Figure 31.

TYPICAL CHARACTERISTICS (continued)

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.

LARGE-SIGNAL STEP RESPONSE

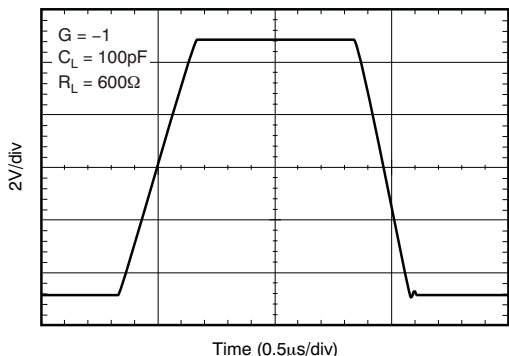


Figure 32.

LARGE-SIGNAL STEP RESPONSE

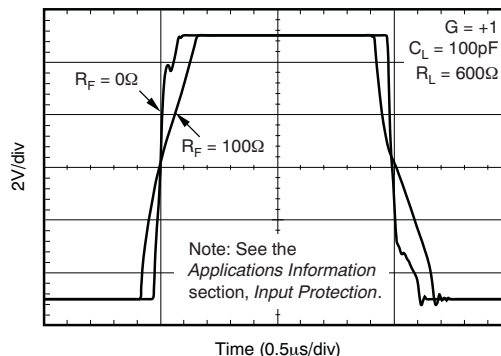


Figure 33.

LARGE-SIGNAL POSITIVE SETTLING TIME (10V_{PP}, C_L = 100pF)

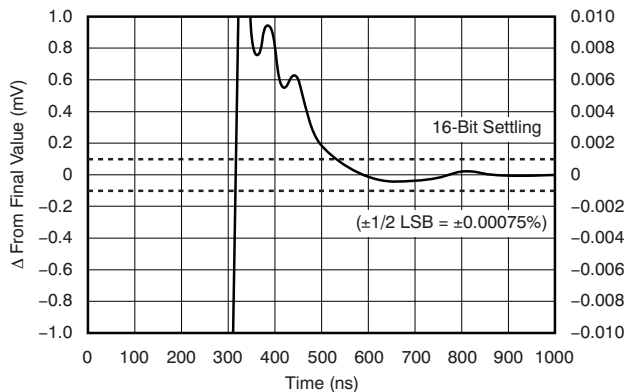


Figure 34.

LARGE-SIGNAL POSITIVE SETTLING TIME (10V_{PP}, C_L = 10pF)

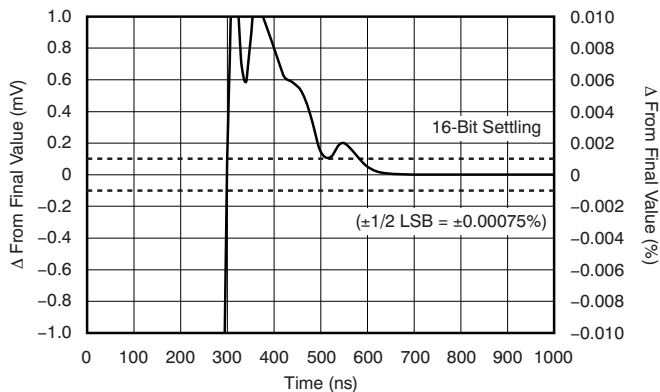


Figure 35.

LARGE-SIGNAL NEGATIVE SETTLING TIME (10V_{PP}, C_L = 100pF)

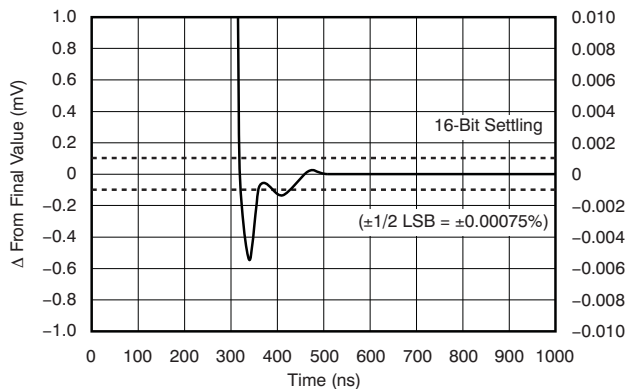


Figure 36.

LARGE-SIGNAL NEGATIVE SETTLING TIME (10V_{PP}, C_L = 10pF)

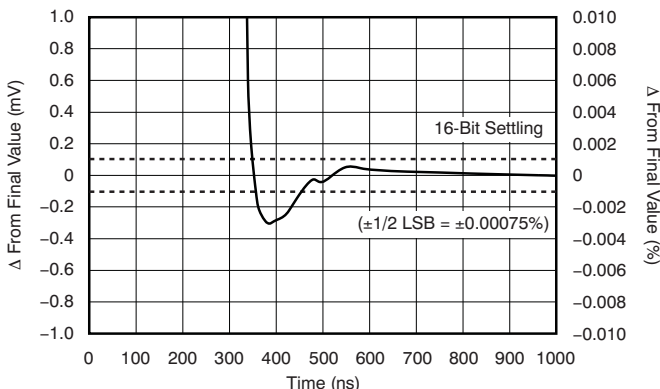


Figure 37.

TYPICAL CHARACTERISTICS (continued)

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.

NEGATIVE OVERLOAD RECOVERY

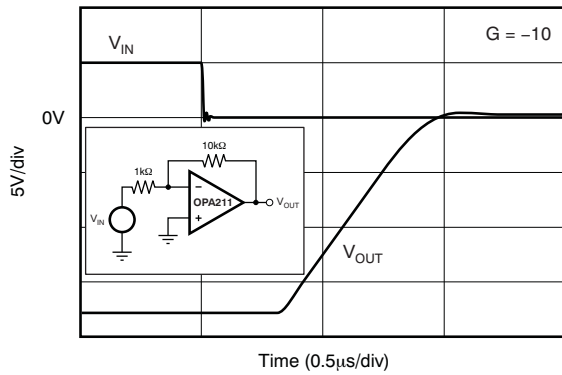


Figure 38.

POSITIVE OVERLOAD RECOVERY

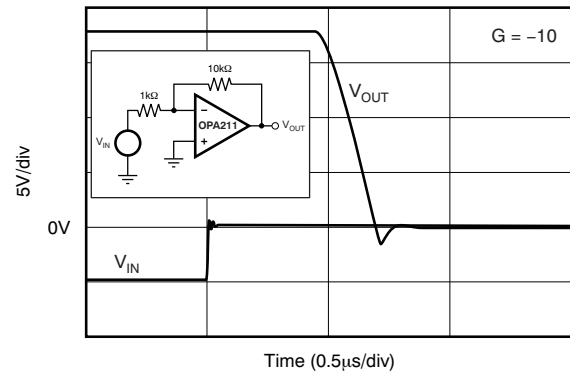


Figure 39.

OUTPUT VOLTAGE vs OUTPUT CURRENT

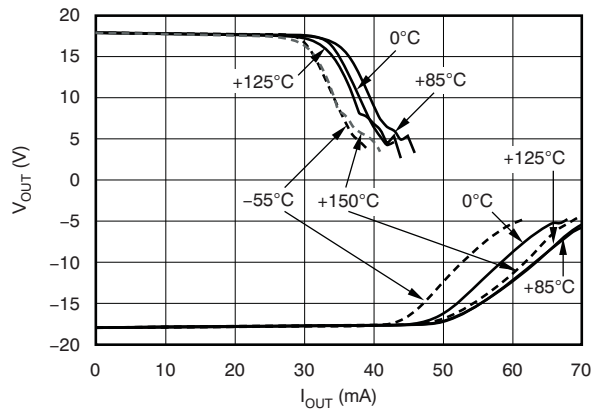


Figure 40.

NO PHASE REVERSAL

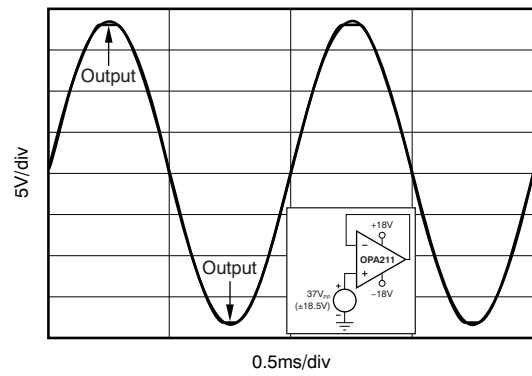


Figure 41.

TURN-OFF TRANSIENT

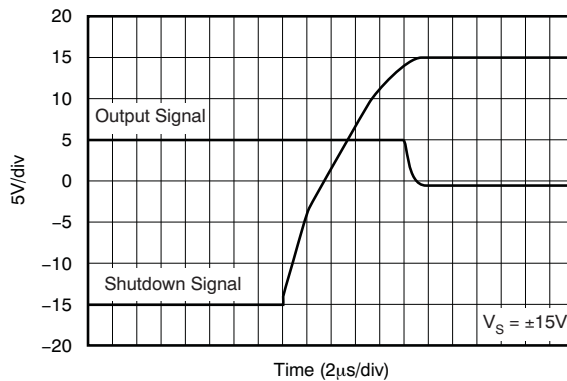


Figure 42.

TURN-ON TRANSIENT

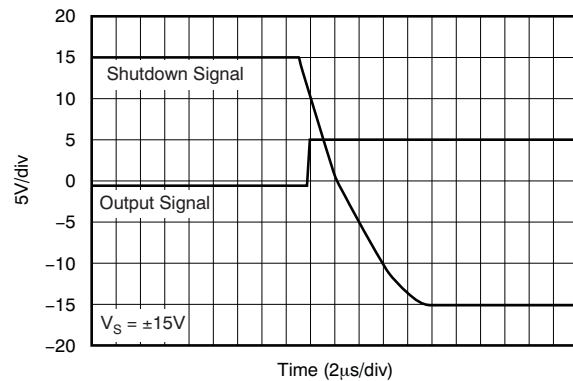


Figure 43.

TYPICAL CHARACTERISTICS (continued)

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.

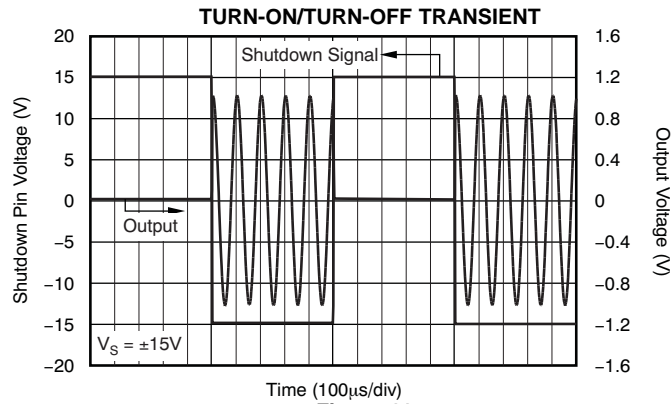


Figure 44.

APPLICATION INFORMATION

The OPA211 is a unity-gain stable, precision op amp with very low noise. Applications with noisy or high-impedance power supplies require decoupling capacitors close to the device pins. In most cases, 0.1 μ F capacitors are adequate. [Figure 45](#) shows a simplified schematic of the OPA211. This die uses a SiGe bipolar process and contains 180 transistors.

OPERATING VOLTAGE

OPA211 series op amps operate from $\pm 2.25\text{V}$ to $\pm 18\text{V}$ supplies while maintaining excellent performance. The OPA211 series can operate with as little as +4.5V between the supplies and with up to +36V between the supplies. However, some applications do not require equal positive and

negative output voltage swing. With the OPA211 series, power-supply voltages do not need to be equal. For example, the positive supply could be set to +25V with the negative supply at -5V or vice-versa.

The common-mode voltage must be maintained within the specified range. In addition, key parameters are assured over the specified temperature range, $T_A = -55^\circ\text{C}$ to $+125^\circ\text{C}$. Parameters that vary significantly with operating voltage or temperature are shown in the [Typical Characteristics](#).

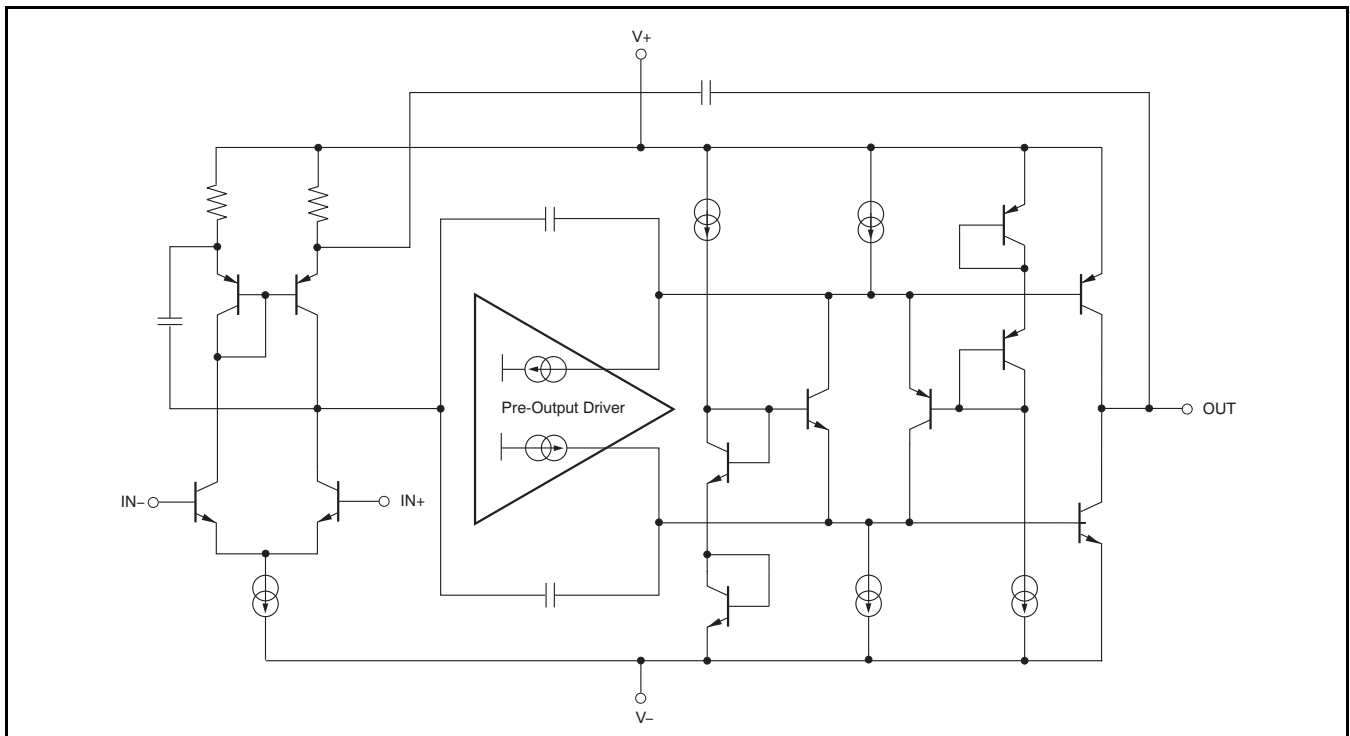


Figure 45. OPA211 Simplified Schematic

INPUT PROTECTION

The input terminals of the OPA211 are protected from excessive differential voltage with back-to-back diodes, as shown in Figure 46. In most circuit applications, the input protection circuitry has no consequence. However, in low-gain or $G = 1$ circuits, fast ramping input signals can forward bias these diodes because the output of the amplifier cannot respond rapidly enough to the input ramp. This effect is illustrated in Figure 33 of the Typical Characteristics. If the input signal is fast enough to create this forward bias condition, the input signal current must be limited to 10mA or less. If the input signal current is not inherently limited, an input series resistor can be used to limit the signal input current. This input series resistor degrades the low-noise performance of the OPA211, and is discussed in the *Noise Performance* section of this data sheet. Figure 46 shows an example implementing a current-limiting feedback resistor.

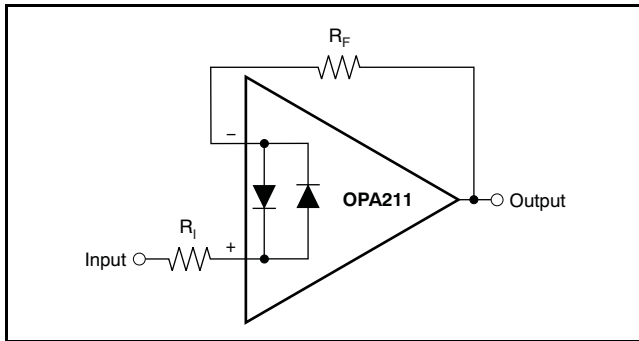


Figure 46. Pulsed Operation

NOISE PERFORMANCE

Figure 47 shows total circuit noise for varying source impedances with the op amp in a unity-gain configuration (no feedback resistor network, and therefore no additional noise contributions). Two different op amps are shown with total circuit noise calculated. The OPA211 has very low voltage noise, making it ideal for low source impedances (less than 2k Ω). A similar precision op amp, the OPA227, has somewhat higher voltage noise but lower current noise. It provides excellent noise performance at moderate source impedance (10k Ω to 100k Ω). Above 100k Ω , a FET-input op amp such as the OPA132 (very low current noise) may provide improved performance. The equation in Figure 47 is shown for the calculation of the total circuit noise. Note that e_n = voltage noise, i_n = current noise, R_S = source impedance, k = Boltzmann's constant = 1.38×10^{-23} J/K, and T is temperature in K.

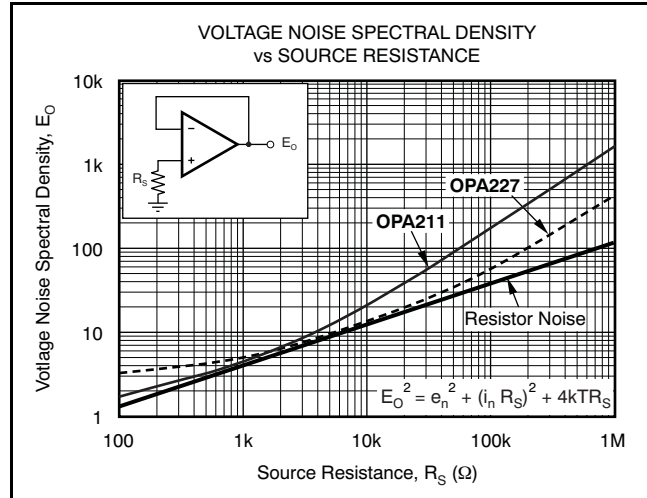


Figure 47. Noise Performance of the OPA211 and OPA227 in Unity-Gain Buffer Configuration

BASIC NOISE CALCULATIONS

Design of low-noise op amp circuits requires careful consideration of a variety of possible noise contributors: noise from the signal source, noise generated in the op amp, and noise from the feedback network resistors. The total noise of the circuit is the root-sum-square combination of all noise components.

The resistive portion of the source impedance produces thermal noise proportional to the square root of the resistance. This function is plotted in Figure 47. The source impedance is usually fixed; consequently, select the op amp and the feedback resistors to minimize the respective contributions to the total noise.

Figure 47 depicts total noise for varying source impedances with the op amp in a unity-gain configuration (no feedback resistor network, and therefore no additional noise contributions). The operational amplifier itself contributes both a voltage noise component and a current noise component. The voltage noise is commonly modeled as a time-varying component of the offset voltage. The current noise is modeled as the time-varying component of the input bias current and reacts with the source resistance to create a voltage component of noise. Therefore, the lowest noise op amp for a given application depends on the source impedance. For low source impedance, current noise is negligible and voltage noise generally dominates. For high source impedance, current noise may dominate.

Figure 48 illustrates both inverting and noninverting op amp circuit configurations with gain. In circuit configurations with gain, the feedback network resistors also contribute noise. The current noise of the op amp reacts with the feedback resistors to create additional noise components. The feedback resistor values can generally be chosen to make these noise sources negligible. The equations for total noise are shown for both configurations.

TOTAL HARMONIC DISTORTION MEASUREMENTS

OPA211 series op amps have excellent distortion characteristics. THD + Noise is below 0.0002% ($G = +1$, $V_{OUT} = 3V_{RMS}$) throughout the audio frequency range, 20Hz to 20kHz, with a 600Ω load.

The distortion produced by OPA211 series op amps is below the measurement limit of many commercially available distortion analyzers. However, a special test circuit illustrated in Figure 49 can be used to extend the measurement capabilities.

Op amp distortion can be considered an internal error source that can be referred to the input. Figure 49 shows a circuit that causes the op amp distortion to be 101 times greater than that normally produced by the op amp. The addition of R_3 to the otherwise standard noninverting amplifier configuration alters the feedback factor or noise gain of the circuit. The closed-loop gain is unchanged, but the feedback available for error correction is reduced by a factor of

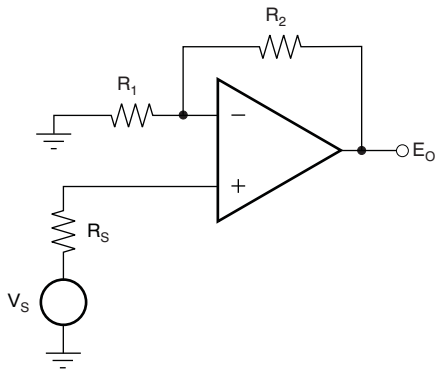
101, thus extending the resolution by 101. Note that the input signal and load applied to the op amp are the same as with conventional feedback without R_3 . The value of R_3 should be kept small to minimize its effect on the distortion measurements.

Validity of this technique can be verified by duplicating measurements at high gain and/or high frequency where the distortion is within the measurement capability of the test equipment. Measurements for this data sheet were made with an Audio Precision System Two distortion/noise analyzer, which greatly simplifies such repetitive measurements. The measurement technique can, however, be performed with manual distortion measurement instruments.

SHUTDOWN

The shutdown (enable) function of the OPA211 is referenced to the positive supply voltage of the operational amplifier. A valid high disables the op amp. A valid high is defined as $(V+) - 0.35V$ of the positive supply applied to the shutdown pin. A valid low is defined as $(V+) - 3V$ below the positive supply pin. For example, with V_{CC} at $\pm 15V$, the device is enabled at or below 12V. The device is disabled at or above 14.65V. If dual or split power supplies are used, care should be taken to ensure the valid high or valid low input signals are properly referred to the positive supply voltage. This pin must be connected to a valid high or low voltage or driven, and not left open-circuit. The enable and disable times are provided in the Typical Characteristics section (see Figure 42 through Figure 44). When disabled, the output assumes a high-impedance state.

Noise in Noninverting Gain Configuration



Noise at the output:

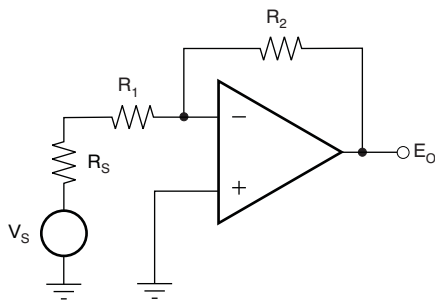
$$E_O^2 = \left(1 + \frac{R_2}{R_1} \right)^2 e_n^2 + e_1^2 + e_2^2 + (i_n R_2)^2 + e_s^2 + (i_n R_S)^2 \left(1 + \frac{R_2}{R_1} \right)^2$$

Where $e_s = \sqrt{4kTR_S} \times \left(1 + \frac{R_2}{R_1} \right)$ = thermal noise of R_S

$e_1 = \sqrt{4kTR_1} \times \left(\frac{R_2}{R_1} \right)$ = thermal noise of R_1

$e_2 = \sqrt{4kTR_2}$ = thermal noise of R_2

Noise in Inverting Gain Configuration



Noise at the output:

$$E_O^2 = \left(1 + \frac{R_2}{R_1 + R_S} \right)^2 e_n^2 + e_1^2 + e_2^2 + (i_n R_2)^2 + e_s^2$$

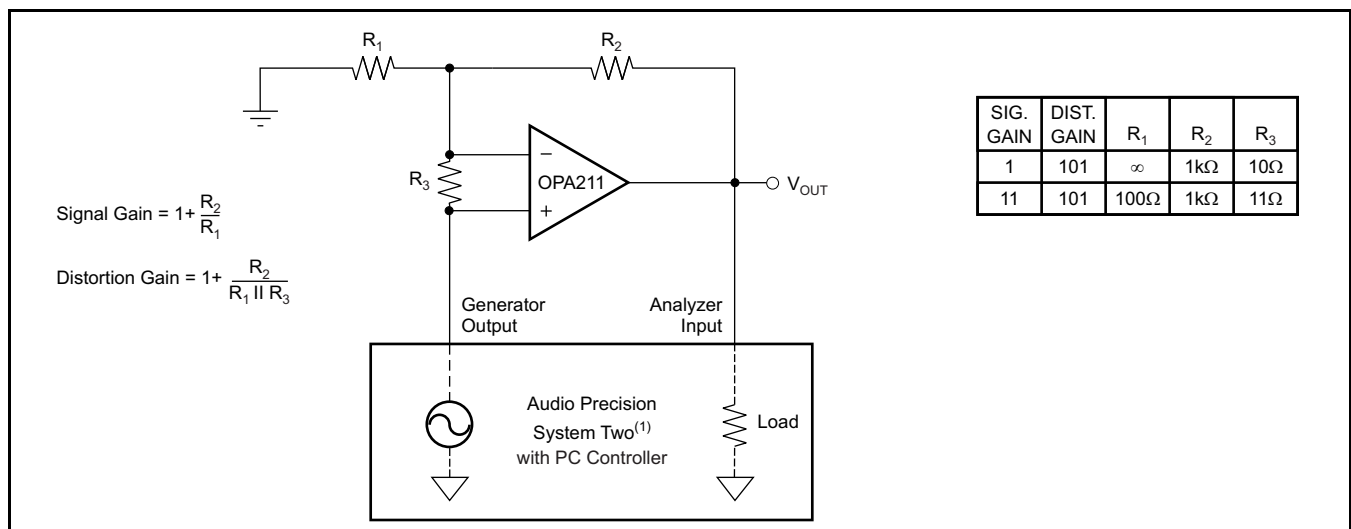
Where $e_s = \sqrt{4kTR_S} \times \left(\frac{R_2}{R_1 + R_S} \right)$ = thermal noise of R_S

$e_1 = \sqrt{4kTR_1} \times \left(\frac{R_2}{R_1 + R_S} \right)$ = thermal noise of R_1

$e_2 = \sqrt{4kTR_2}$ = thermal noise of R_2

For the OPA211 series op amps at 1kHz, $e_n = 1.1\text{nV}/\sqrt{\text{Hz}}$ and $i_n = 1.7\text{pA}/\sqrt{\text{Hz}}$.

Figure 48. Noise Calculation in Gain Configurations



(1) For measurement bandwidth, see [Figure 4](#), [Figure 5](#), and [Figure 6](#).

Figure 49. Distortion Test Circuit

ELECTRICAL OVERSTRESS

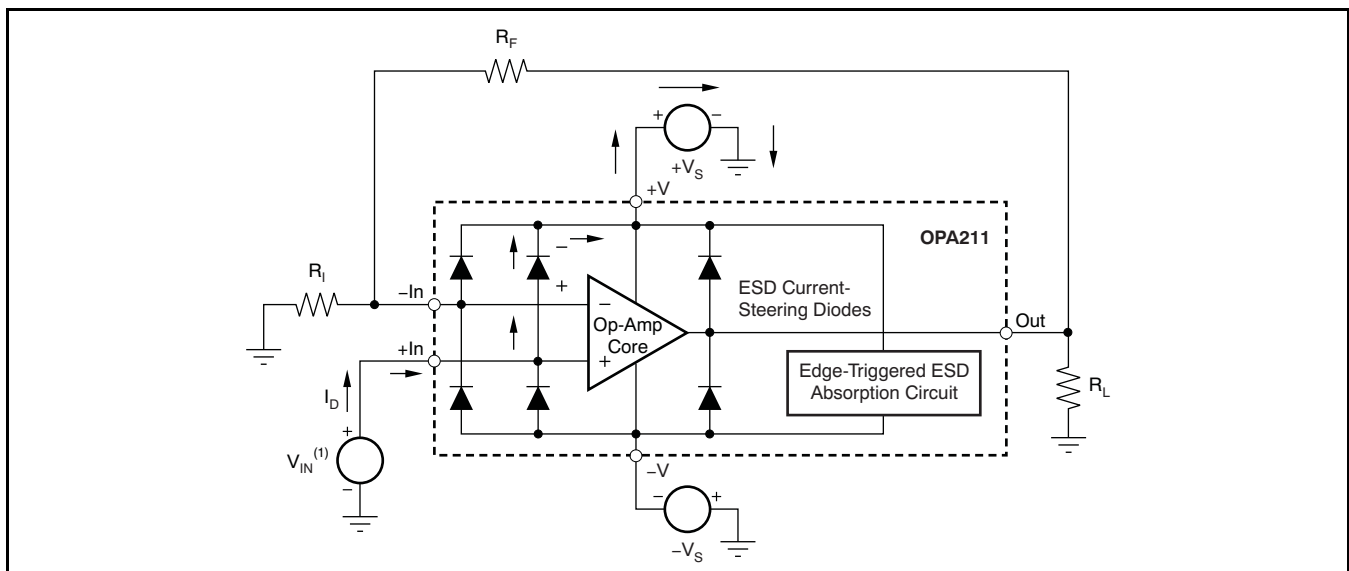
Designers often ask questions about the capability of an operational amplifier to withstand electrical overstress. These questions tend to focus on the device inputs, but may involve the supply voltage pins or even the output pin. Each of these different pin functions have electrical stress limits determined by the voltage breakdown characteristics of the particular semiconductor fabrication process and specific circuits connected to the pin. Additionally, internal electrostatic discharge (ESD) protection is built into these circuits to protect them from accidental ESD events both before and during product assembly.

It is helpful to have a good understanding of this basic ESD circuitry and its relevance to an electrical overstress event. Figure 50 illustrates the ESD circuits contained in the OPA211 (indicated by the dashed line area). The ESD protection circuitry involves several current-steering diodes connected from the input and output pins and routed back to the internal power-supply lines, where they meet at an absorption device internal to the operational amplifier. This protection circuitry is intended to remain inactive during normal circuit operation.

An ESD event produces a short duration, high-voltage pulse that is transformed into a short duration, high-current pulse as it discharges through a semiconductor device. The ESD protection circuits are designed to provide a current path around the operational amplifier core to prevent it from being damaged. The energy absorbed by the protection circuitry is then dissipated as heat.

When an ESD voltage develops across two or more of the amplifier device pins, current flows through one or more of the steering diodes. Depending on the path that the current takes, the absorption device may activate. The absorption device has a trigger, or threshold voltage, that is above the normal operating voltage of the OPA211 but below the device breakdown voltage level. Once this threshold is exceeded, the absorption device quickly activates and clamps the voltage across the supply rails to a safe level.

When the operational amplifier connects into a circuit such as that illustrated in Figure 50, the ESD protection components are intended to remain inactive and not become involved in the application circuit operation. However, circumstances may arise where an applied voltage exceeds the operating voltage range of a given pin. Should this condition occur, there is a risk that some of the internal ESD protection circuits may be biased on, and conduct current. Any such current flow occurs through steering diode paths and rarely involves the absorption device.



(1) $V_{IN} = +V_S + 500\text{mV}$.

Figure 50. Equivalent Internal ESD Circuitry and Its Relation to a Typical Circuit Application

Figure 50 depicts a specific example where the input voltage, V_{IN} , exceeds the positive supply voltage ($+V_S$) by 500mV or more. Much of what happens in the circuit depends on the supply characteristics. If $+V_S$ can sink the current, one of the upper input steering diodes conducts and directs current to $+V_S$. Excessively high current levels can flow with increasingly higher V_{IN} . As a result, the datasheet specifications recommend that applications limit the input current to 10mA.

If the supply is not capable of sinking the current, V_{IN} may begin sourcing current to the operational amplifier, and then take over as the source of positive supply voltage. The danger in this case is that the voltage can rise to levels that exceed the operational amplifier absolute maximum ratings. In extreme but rare cases, the absorption device triggers on while $+V_S$ and $-V_S$ are applied. If this event happens, a direct current path is established between the $+V_S$ and $-V_S$ supplies. The power dissipation of the absorption device is quickly exceeded, and the extreme internal heating destroys the operational amplifier.

Another common question involves what happens to the amplifier if an input signal is applied to the input while the power supplies $+V_S$ and/or $-V_S$ are at 0V. Again, it depends on the supply characteristic while at 0V, or at a level below the input signal amplitude. If

the supplies appear as high impedance, then the operational amplifier supply current may be supplied by the input source via the current steering diodes. This state is not a normal bias condition; the amplifier most likely will not operate normally. If the supplies are low impedance, then the current through the steering diodes can become quite high. The current level depends on the ability of the input source to deliver current, and any resistance in the input path.

THERMAL CONSIDERATIONS

The primary issue with all semiconductor devices is junction temperature (T_J). The most obvious consideration is assuring that T_J never exceeds the absolute maximum rating specified for the device. However, addressing device thermal dissipation has benefits beyond protecting the device from damage. Even modest increases in junction temperature can decrease op amp performance, and temperature-related errors can accumulate. Understanding the power generated by the device within the specific application and assessing the thermal effects on the error tolerance lead to a better understanding of system performance and thermal dissipation needs.

PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
OPA211MDGKTEP	ACTIVE	VSSOP	DGK	8	250	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-55 to 125	OBCM	Samples
V62/12619-01XE	ACTIVE	VSSOP	DGK	8	250	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-55 to 125	OBCM	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

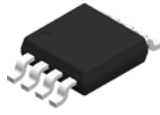
(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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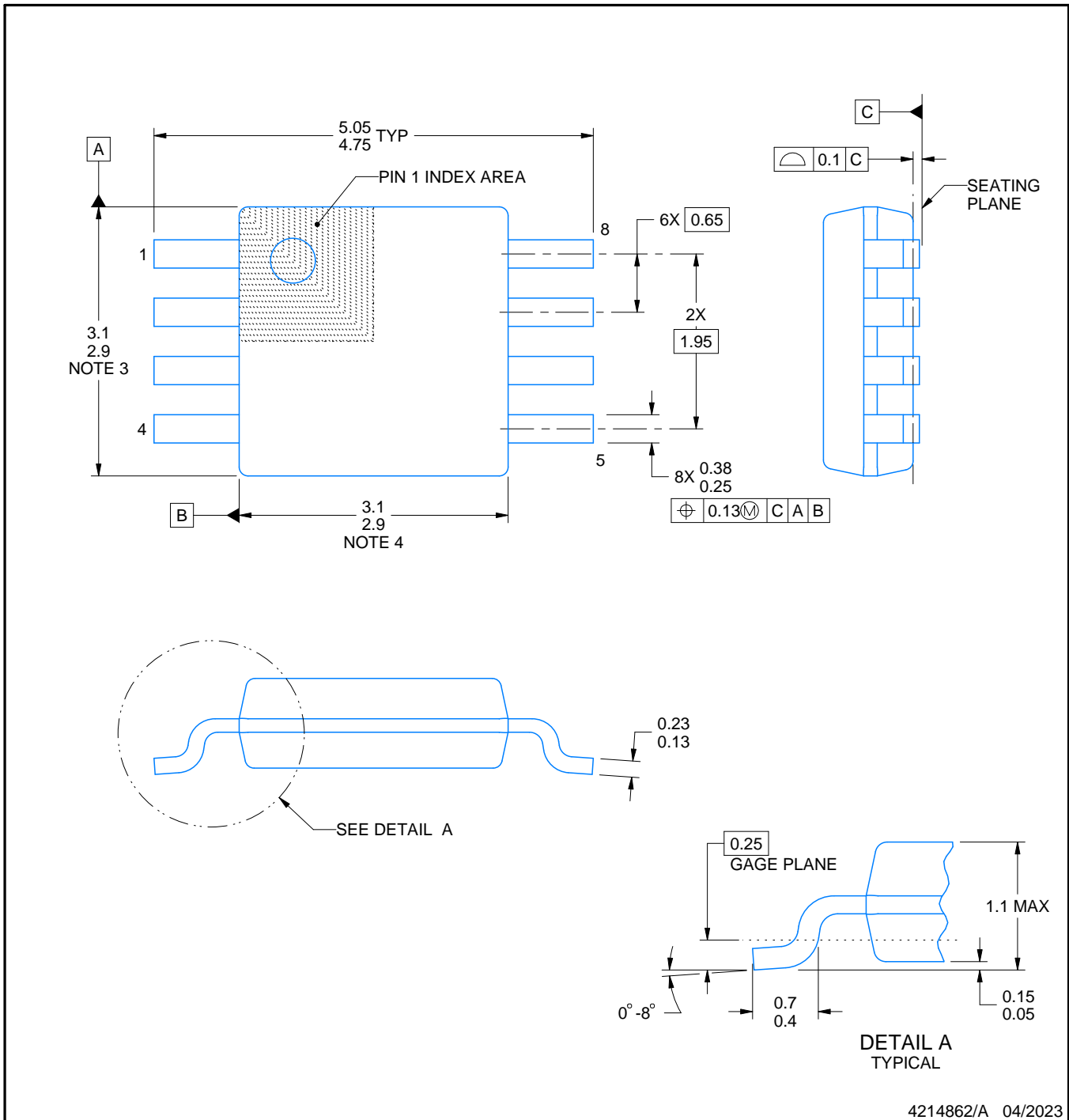
DGK0008A



PACKAGE OUTLINE

VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



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NOTES:

PowerPAD is a trademark of Texas Instruments.

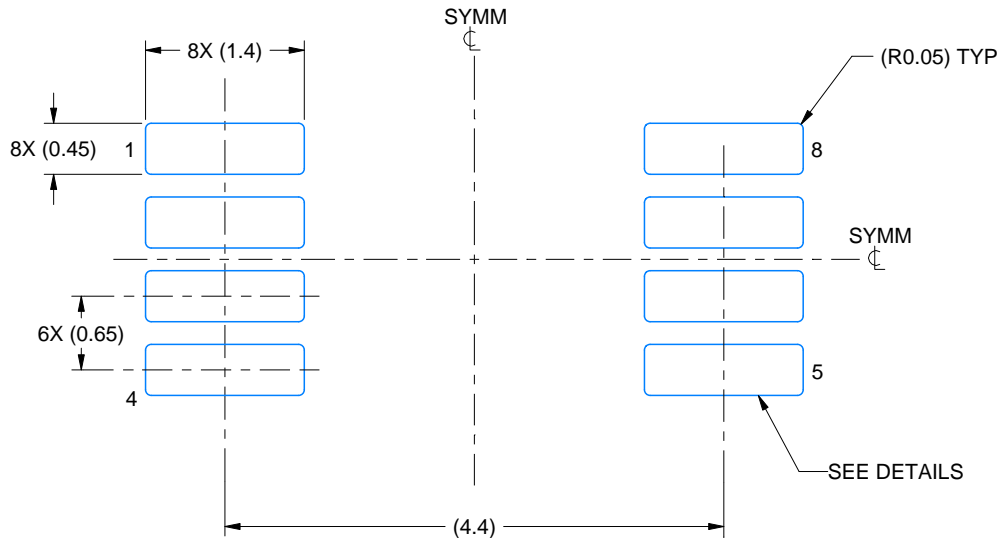
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
5. Reference JEDEC registration MO-187.

EXAMPLE BOARD LAYOUT

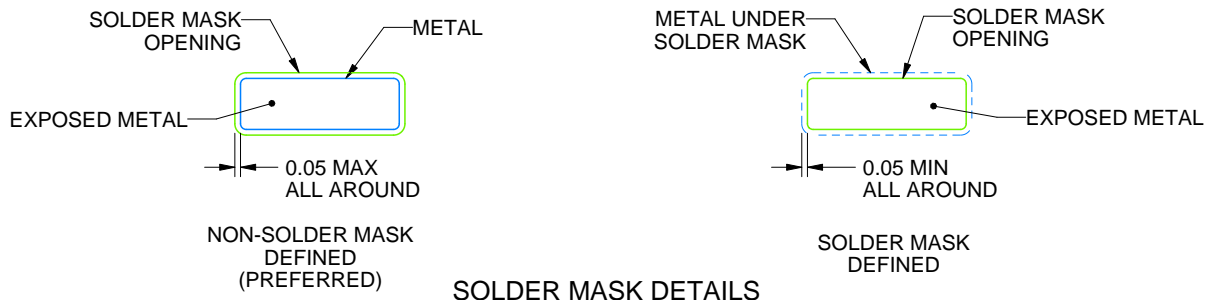
DGK0008A

™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE: 15X



SOLDER MASK DETAILS

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NOTES: (continued)

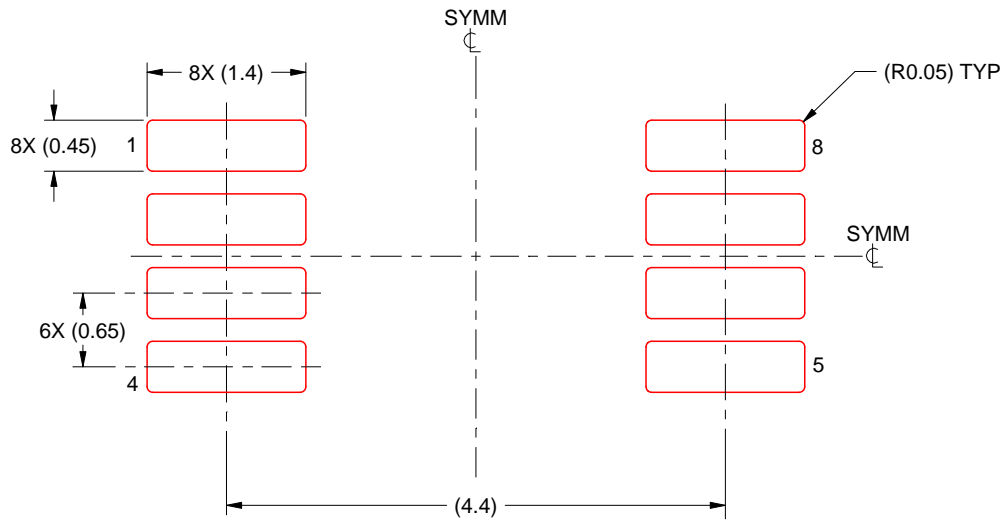
6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
9. Size of metal pad may vary due to creepage requirement.

EXAMPLE STENCIL DESIGN

DGK0008A

™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



SOLDER PASTE EXAMPLE
SCALE: 15X

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NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
12. Board assembly site may have different recommendations for stencil design.

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